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Sensor apparatus for determination of the tire internal  
pressure for a motor vehicle

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The invention relates to a sensor apparatus for  
determination of the tire internal pressure for a motor  
vehicle by means of at least one measurement sensor in  
the form of an optical fiber, with the sought  
10 parameter being deduced from the change in the light  
wave.

DE 39 37 966 C2 has already disclosed sensor  
apparatuses such as these, in which at least one sensor  
15 detects the locally occurring deformation. Sensors are  
fitted in the area of the tread of the tire. This  
arrangement makes use of radio transmission of the  
measured signals from a transmitter that is arranged in  
the vehicle wheel to a receiver within the vehicle  
20 structure. The values are determined, for example, by  
means of strain gauges which are vulcanized into the  
tires. This is intended to allow determination not only  
of the tire pressure but also of longitudinal and  
lateral forces acting on the tire. The introduction of  
25 the measurement sensors into the tires in its own right  
results in considerable problems in tire manufacture.

In order to overcome the problems of the abovementioned  
sensor apparatus, a vehicle tire sensor apparatus which  
30 has been disclosed in DE 102 08 998 A1 uses a  
measurement sensor for determination of widely  
differing parameters relating to a tire. This  
measurement sensor is in the form of an optical fiber,  
by means of which a light wave is passed through the  
35 tire circumference. The respective changes in the  
reflection and transmission characteristics of the  
light wave allow conclusions to be drawn about the tire  
parameter or parameters sought. The use of optical  
measurement sensors such as these results in

extraordinarily little complexity in tire manufacture. The already known apparatus preferably uses infrared light from the available spectral range, thus considerably reducing the damaging influence on the  
5 tire material. The use of a sensor apparatus such as this is relatively versatile.

Nevertheless efforts are being made to advantageously develop further possible applications. Particular  
10 attention is being paid to the problem of determining in particular the tire internal pressure.

Nowadays, a large number of special monitoring systems are used for measurement of the tire internal pressure,  
15 and in practice result in considerable technical complexity and significant costs.

Various monitoring systems are known for monitoring the tire internal pressure, for example those which are  
20 fitted in the rim and measure the tire pressure directly or else others which use an ABS sensor system to detect any change in the rolling circumference of the tire and in this way allow conclusions to be drawn about any pressure loss.

25 The object of the invention is therefore to provide a sensor apparatus for determination of a tire internal pressure for a motor vehicle of the type defined in more detail in the introduction, by means of which  
30 sensor apparatus the internal pressure of a tire can be determined in a manner which is technically as simple as possible, and cost-effective.

The invention makes use of the principle of  
35 determination of a tire internal pressure on the basis of tire deformation. If an already-known fiber sensor system is used as the measurement sensor for measurement, then it can be used directly for

monitoring the tire internal pressure without any additional special sensors being required.

5 According to the invention, in the case of a sensor apparatus of the type referred to in the introduction, the arrangement is designed such that the measurement sensor determines the shape and/or size of the tire contact area as an indicator of the internal pressure. The shape and size of the tire contact area on the  
10 roadway are dependent on the wheel load, which fluctuates all the time while driving. However, its mean value does not fluctuate.

The influence of the wheel load on the tire internal  
15 pressure can, however, be eliminated by appropriately configured low-pass filtering in one advantageous embodiment of the invention.

If required, further data can be used to take account  
20 of wheel load changes, such as the vehicle longitudinal acceleration, the vehicle lateral acceleration, the speed and the tank volume. These contribute significantly to consideration to the changes in the wheel loads. Low-pass filtered evaluation in its own  
25 right allows a slow loss of air to be detected.

Air pressure and wheel load also determine the size and shape of the tire contact area. For example, a particularly high air pressure can lead to a fairly  
30 round contact area shape. This corresponds to an increased supporting component of the tread in the tire center.

The tire curvature transverse with respect to the  
35 direction of travel within and outside the tire contact area can also be used to determine the tire internal pressure.

The determination of the tire internal pressure by means of the tire deformation as an indicator has the advantage, particularly when using existing fiber-optic sensor systems, that there is thus no need for a  
5 special tire pressure monitoring system.

As a result of the use of optical fibers, the invention allows simple signal transmission to an evaluation and computer unit which is provided in the vehicle  
10 structure.

In principle, an optical coupler which is centered axially in the wheel is suitable for transmission of the light signal emitted from the measurement sensor to  
15 the evaluation and computer unit in the vehicle structure.

Since it can be complex in practice to pass the fiber out of the tire in conjunction with optical  
20 transmission from the rotating fiber to a non-rotating fiber in the wheel hub, it is advantageous to also vulcanize an optoelectronic evaluation unit into the tread of the tire.

25 A unit which has been vulcanized in such a way satisfies the requirements for compactness, weight and mechanical load capacity when, for example, it has at most a diameter of approximately 30 mm, a thickness of about 2 mm and a weight of about 10 g.

30 In one advantageous embodiment of the invention, an evaluation unit for fiber-optic Bragg grating systems can be used, in which the wavelength is determined by means of passive edge filters on three independent  
35 channels. A superluminescent diode (SLD) can be used as a light source. The evaluation unit may be formed from standard components, which are soldered on a board. Integration of the various components directly in the silicon material makes it possible to considerably

reduce the required physical space further, and at the same time to increase the mechanical load capacity.

The sensor apparatus according to the invention can also be provided by means of so-called ASIC (active silicon integrated circuit) technology, with optical conductor tracks being produced directly in the silicon, and light sources and photodetectors being fitted. In this case, the evaluation unit is preferably in the form of a superluminescent diode (SLD) light source and a photo diode with a Mach-Zehnder interferometer for wavelength determination. In this case, the interferometer operates without any moving parts. The difference in the optical path length is produced by splitting the arriving light between two optical conductor tracks whose refractive index can be varied by electrical application of charge carriers. Since all of the required parts can be integrated in one chip, the mechanical load capacity of a system such as this is very high.

An electrical power demand for the evaluation unit of, for example, up to 1 W in the tire can be coped with by known systems, with a measurement cycle in this power range requiring a few nanoseconds.

The fact that the flexing work which has to be carried out by the tire material increases as the tire pressure decreases, particularly in the area of the tire contact area affects the fuel consumption in the same way as the risk of future tire damage. In order to take precautions against these phenomena, and, if required, as an alternative or additional option for determination of the tire internal pressure it is possible to detect the flexing work. The flexing work can in this case be detected simply by measurement of the tire temperature, for example, by means of fiber Bragg gratings (FBGs).

The invention accordingly provides for the tire temperature to be measured continuously by means of a temperature sensor, for tire heating to be detected and for flexing work to be estimated, in order to determine  
5 the difference between a nominal pressure and an actual pressure, and to avoid tire damage resulting from overheating.

Further features, details and advantages of the  
10 invention will become evident from the description, the patent claims and the drawing.

One exemplary embodiment of the sensor apparatus according to the invention for determination of a tire  
15 internal pressure for a motor vehicle is illustrated in the drawing and will be explained in more detail in the following text.

In the drawing:

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Figure 1 shows a schematic detail of the cross section through a tire of a motor vehicle with a sensor apparatus according to the invention;

25 Figure 2 shows a schematic plan view of the tread of the tire;

Figure 3 shows a block diagram of the sensor apparatus;

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Figures 4a to 4c each show a graph with a tire contact area and a longitudinal slip movement distribution in three different state ranges; and

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Figure 5 shows the determination of surface strain from measured longitudinal slip movements, as shown in Figures 4a to 4c, in the tire contact area.

Figure 1 shows a tire 2 which has been pulled on to a rim 1. This tire has a tread 3 whose profile is illustrated in more detail schematically in figure 2.

5 The tire 2 is formed in the conventional manner with a belt, a binding and further fabric and reinforcing layers 4. A plurality of optical fibers 6 are embedded in the area of the tread 3 in the tire, run around the tire circumference and are part of a sensor apparatus 5

10 for determination of the tire internal pressure.

Only two such fibers 6 are indicated, by way of example, on the tread 3 in Figure 2. The refractive index of the optical fibers varies at a sensor element

15 with a corresponding grating constant, that is to say, it varies at the sensor element in a periodic interval between two refractive index values. The optical fibers 6 are laid unstressed, that is to say they are neither stretched nor compressed.

20 In contrast to the illustrated embodiment, the optical fibers 6 may, of course, also alternatively or in addition to the arrangement on the tread 3 be fitted to a shoulder or a side wall 7 of the tire 2.

25 As is shown in a highly abstracted manner and in the form of a block diagram, in Figure 3, a signal transmitter 9 is provided on the vehicle structure 8, or may, for example, be in the form of an infrared

30 light-transmitting light-emitting diode or an infrared laser. The incoming light signal is fed via a coupler 10, which is arranged in the wheel or directly on the tire, into the optical fibers 6 which are arranged on the tire 2. The output light signal, which varies as a

35 result of the tire deformation at the sensor elements, is supplied via the coupler 10 to an evaluation and computer unit 11.

The arrangement of a plurality of optical fibers 6 or a plurality of sections of a fiber alongside one another, if required even in a plurality of planes, allows numerous individual sensors elements to be fitted in the tire, by means of which it is possible to determine not only the tire contact area but also further parameters. In fact, a plurality of sensor elements such as these can also be used to determine only the shape and/or size of the tire contact area.

The graphs shown in Figures 4a to Figure 4c qualitatively show how a contact area image varies and thus how the shape and/or size of the tire contact area which govern the determination of the tire internal pressure according to the invention vary in different operating states.

Figure 4a shows a tire contact area image of the tire on the basis of a longitudinal slip movement distribution when the vehicle is being braked at a speed of 60 km/h, with a longitudinal slip movement LS in millimeters being shown plotted against a length L in centimeters and a tire width B in centimeters.

In a corresponding manner, the longitudinal slip movement distribution is shown in Figure 4b for a vehicle in a freely rolling state at a vehicle speed of 60 km/h, while Figure 4c shows the vehicle in a driven state at a speed of 60 km/h.

The physical change in the respective longitudinal slip movement corresponds to surface strain and at the same time strain of the optical fibers 6 which are affected by it.

The strain which occurs on the surface of the tread can be determined by formation of the differential quotient along a respective path S which is shown in Figure 4a to Figure 4c, of a longitudinal slip movement.



Figure 5 shows, in the form of a graph, this differentiation for determination of the surface strain from measured longitudinal slip movements, with S1 indicating the freely rolling state, S2 the driven state and S3 the braked state. The braked state shown by the line S3 is in this case illustrated with reversed mathematical signs.

10 When the wheel is rolling freely, only a small amount of strain can be seen from the tire contact area impression. When the wheel is being driven, this strain is considerably greater. In addition, a further strain occurs at the end of the tire contact area. In  
15 contrast, when the vehicle is being braked compression can be seen in the rear contact area. Further investigations have shown that this statement is independent of the speed.

20 Conversely, it is in turn possible to use the measured strains to deduce the profile deflection, by integration and thus to detect how the entire tire contact area is split into adhesion areas and sliding areas. The ratio of the sizes of these two areas then  
25 makes it possible to deduce the current utilization level of the prevailing friction contact potential of the tire contact area.

An addition to the described determination of the tire  
30 internal pressure by measurement of the tire contact area size, the tire temperature is measured continuously by means of a temperature sensor 12 in the illustrated embodiment, so that tire heating can be detected and any flexing work can be estimated. In this  
35 way, it is possible to determine any difference between a nominal pressure and an actual pressure. This additionally makes it possible to prevent tire damage caused by overheating of the tire.